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ADEQUACY OF MACHINING ACCURACY MODELS IN MULTI-TOOL TWO-CARRIAGE SETUPS

Abstract. *The paper demonstrates the adequacy of the developed machining accuracy models in multi-tool two-carriage setups in relation to real machining processes. It is also shown that the developed models enable the prediction of machining accuracy under given conditions (setup structure, properties of the technological system, machining conditions), thereby forming a methodological basis for CAD systems of multi-tool two-carriage lathe machining.*

Introduction. Based on the analysis of multi-tool setups and their implementation methods [1-27], a set of mathematical models of dimensional errors has been developed [28–38]. This set of models covers practically the entire range of setups and methods for implementing multi-tool machining, both on conventional automatic and semi-automatic lathes with cam-controlled systems and on modern CNC multi-purpose lathes of the turning group.

Each model has its own domain of effective application. For instance, for models describing dimensional distortion, which are relatively simple in terms of error formation mechanisms, a set of standard analytical models has been developed for the main classes of multi-tool setups, oriented toward different groups of lathe automation equipment [39–88].

Mathematical models of dimensional distortion and dispersion fields in various types of setups take into account all major sources of machining errors: allowance (depth of cut, t) and its variations, Δt ; stiffness of the technological system, e_0 , e_i , e_{0i} , $i=1\dots n$ and its dispersion, Δe_0 , Δe_i , Δe_{0i} , $i=1\dots n$; strength properties of the workpiece material (through relevant parameters C_x , C_y , C_z) and their instability v ; cutting conditions such as feed (S) and cutting speed (V); cutting tools, material group, and type of machining (C_x , C_y , C_z , x_x , x_y , x_z).

Such a wide range of considered factors makes the developed models a powerful tool for analyzing and predicting machining accuracy.

The developed set of mathematical models of dimensional errors in multi-tool setups forms the basis of the theory of multi-tool machining accuracy [89–122]. Due

to the significantly different levels of complexity of the developed models, the following scheme of their application is recommended:

- simpler standard models oriented to specific classes of multi-tool setups for particular machine groups are used in developing cutting regime standards;
- more complex generalized analytical models and especially the simulation stochastic model are used as a basis in CAD systems for corresponding operations with multi-tool setups of a general type.

However, before using these models, their validity must first be confirmed.

Main Content. Among the listed factors, the most significant are the depth of cut, its variation, and the instability of the technological system properties, since these are the primary sources of dispersion. Other factors influence the models through the dependence of cutting forces on machining regimes. Therefore, the first stage in assessing model adequacy should be verifying the correct accounting of these key factors[19–26].

The adequacy of the models was evaluated using simulation experiments conducted at two levels.

The first level involved laboratory model experiments. On universal equipment, the machining scheme was simulated, and the influence of cutting forces on dimensional distortion due to parallel and angular displacements of technological system elements was experimentally evaluated.

The second group of experiments was carried out directly under production conditions. Due to the practical impossibility of reconfiguring automatic machines for laboratory samples, this study was performed on real industrial technological processes. The research was based on statistical process control methodology.

The model experiments involved evaluating the influence of key technological factors on the dispersion field and comparing it with calculated values obtained from the developed models. Experimental dependencies were obtained by modeling the dispersion field caused by variations in system stiffness (due to machining workpieces of different diameters on different machines) and variations in cutting forces caused by fluctuations in allowance and material hardness.

To model the dispersion field, two groups of workpieces were manufactured—one with minimum and one with maximum dimensions. The first group had minimal allowance and minimal material hardness, while the second group had maximum allowance and hardness.

The first group was machined in a technological system with maximum stiffness, while the second group was machined under minimum stiffness conditions. Different stiffness levels were simulated by varying the workpiece

overhang: 40 mm for the first group and 90 mm for the second group.

To obtain different hardness levels, the first group of workpieces was heat-treated (heated to 1000°C for three hours), while the second group was left without heat treatment. Experiments were conducted for three types of tools: turning tools, facing tools, and boring tools.

For workpieces from different groups processed under identical cutting conditions, the following were measured:

- for turning tools - external diameters;
- for facing tools - lengths;
- for boring tools - internal diameters.

The actual dispersion field was evaluated based on the differences in corresponding dimensions between the two groups.

Internal diameters were measured using dial indicators, while external diameters and lengths were measured using lever micrometers. Experiments were conducted on turret lathes (models 1B118, 1B125). Tool wear was monitored by measuring the flank wear land.

Table 1 presents the results of one such experiment.

Table 1

Comparison of calculated [19 ,20] and experimental dispersion fields of diameter (40X, HB 2.24 GPa; tool – turning, T15K6, $\gamma = 45^\circ$, $a = 1$ mm; ITZ12; $V = 160$ m/min)

Initial diameter, mm	Cutting mode		Dispersion field, $\Delta\Sigma$ μm		Deviation, %
	S, mm/rev	t, mm	Calculation	experiment	
40	0.26	2	152	145	-5
		4	210	204	-3
36	0.24	2	130	123	-5
		4	216	208	-4
32	0.22	2	103	94	-9
		4	192	204	-6

As shown in Table 1, the adequacy of the models with respect to the main factors of dispersion field formation is high. Therefore, these models can be used for predicting machining accuracy at the design stage.

However, for practical application, the model parameters must correspond to measurable quantities. For example, the model calculates the component of dispersion caused by elastic deformations, while in practice only the total dispersion can be measured. Similarly, instead of depth-of-cut variations, only workpiece dimensional deviations can be measured.

To relate these parameters, a known model of machining error can be used [6]. Its transformation for lathe machining is given as:

$$\Delta_{\Sigma} = \sqrt{(\Delta y)^2 + \Delta_s^2 + \Delta_t^2 + 3(\Sigma \Delta_{CT})^2 + 3(\Sigma \Delta_T)^2} \quad (1)$$

where: Δ_{Σ} - total machining error; Δ_t - tool wear; $\Sigma \Delta_T$ - thermal deformations; $\Sigma \Delta_{CT}$ - geometric errors; Δ_s - setup errors; and Δ_y - elastic deformation errors.

In this model, the corresponding component is determined according to relationships given in [20, 26]. For the remaining components, which do not depend on cutting conditions and therefore can be considered constants under the conditions of the present problem, extensive statistical data are available in the reference literature. Based on these data and standard recommendations, a model can also be proposed for calculating variations in the depth of cut (Δt):

$$\Delta t = TZ + \Delta_s + \Delta_t + \Delta_{CT} \quad (2)$$

where TZ is the tolerance zone of the workpiece for the specified dimension.

With these additions, it becomes possible to perform accuracy analysis of real technological processes and to evaluate the adequacy of the developed dispersion field models under production conditions.

To evaluate real technological processes, statistical process control data from a manufacturing plant were used. The control system was implemented according to GOST 16.305-74.

At the Chelyabinsk Measuring Instruments Plant, setups were analyzed where the loading scheme corresponded to the developed models. Samples were taken at 30-minute intervals, and control charts (\bar{X} -R charts) were constructed. Statistical dispersion limits were compared with calculated values.

The analysis showed that measured dispersion values do not exceed calculated ones and remain within a 12% interval. With a confidence level of 0.95, the measured and calculated accuracies belong to the same statistical population.

Conclusion. Thus, the adequacy of the developed models to real machining processes has been confirmed. Consequently, the developed theory enables prediction of machining accuracy under given conditions (setup structure, technological system properties, machining conditions), forming a methodological basis for CAD systems in multi-tool lathe machining.

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